

# Using the witness method to detect rigid subsystems of geometric constraints in CAD

Dominique Michelucci  
LE2I, UMR CNRS 5158  
Université de Bourgogne  
dmichel@u-bourgogne.fr

Pascal Schreck  
LSIIT, UMR CNRS 7005  
Université de Strasbourg  
schreck@unistra.fr

Simon E.B. Thierry  
LSIIT, UMR CNRS 7005  
Université de Strasbourg  
simon.thierry@unistra.fr

Christoph Fünfzig  
LE2I, UMR CNRS 5158  
Université de Bourgogne  
christoph.fuenfzig@u-bourgogne.fr

Jean-David Genèveux  
LSIIT, UMR CNRS 7005  
Université de Strasbourg  
jean-david.geneveux@etu.unistra.fr

## ABSTRACT

This paper deals with the resolution of geometric constraint systems encountered in CAD-CAM. The main results are that the witness method can be used to detect that a constraint system is over-constrained and that the computation of the maximal rigid subsystems of a system leads to a powerful decomposition method.

In a first step, we recall the theoretical framework of the witness method in geometric constraint solving and extend this method to generate a witness. We show then that it can be used to incrementally detect over-constrainedness. We give an algorithm to efficiently identify all maximal rigid parts of a geometric constraint system. We introduce the algorithm of W-decomposition to identify rigid subsystems: it manages to decompose systems which were not decomposable by classical combinatorial methods.

## Categories and Subject Descriptors

J.6 [Computer Applications]: Computer-Aided Engineering—*Computer-Aided Design*; I.3.5 [Computer Graphics]: Computational Geometry and Object Modeling—*Geometric algorithms, languages, and systems*; G.1.3 [Numerical Analysis]: Numerical Linear Algebra

## Keywords

Geometric Constraints Solving, witness configuration, Jacobian matrix, rigidity theory, W-decomposition

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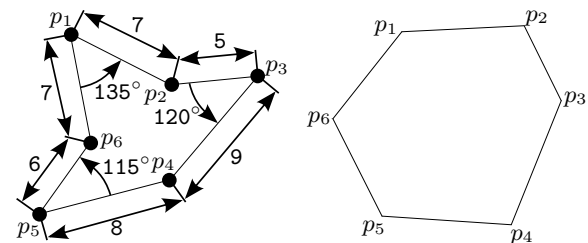


Figure 1: A technical sketch (left) and a possible solution (right).

## 1. INTRODUCTION

Geometric constraints solving in Computer-Aided Design (CAD) aims at yielding a figure which meets some metric requirements (*e.g.* distances between points or angles between lines), usually specified under graphical form. Formally, a geometric constraint system (GCS) consists in constraints (predicates), unknowns (geometric entities) and parameters (metric values). Solutions are returned as the coordinates of the geometric entities. The left of figure 1 shows an example of a technical sketch and its right shows a possible solution.

The literature describes a lot of different approaches to solve geometric constraint systems:

- algebraic methods consist in translating the GCS into a set of equations and working on the equation system, thus forgetting the geometrical background. Algebraic methods can be classified in numerical methods [21] (iterative computations to obtain an approximate solution from initial values given by the user) and symbolic methods [2, 10] (direct computations on the equations – these methods are seldom used because of their complexity),
- geometric methods use the geometric knowledge to solve the system: graph-based methods [6, 21, 9, 28, 29, 31] compile this knowledge in algorithms which consider only combinatorial and connectivity criterions, rule-based methods [16, 3] explicitly use geometric rules to deduce construction plans,
- hybrid methods [4, 8] alternate algebraic and geometric phases of computations to use the powers of both approaches.

For more details on geometric constraint solving, see [11]. A general trend, both to reduce complexity and to enhance resolution power, is to decompose the GCS in solvable subsystems and to assemble their solutions [4, 5, 9, 12, 14, 21, 28, 29, 31, 32, 34]. For instance, on the example of figure 1, it is easy to separately solve each “triangle” ( $p_1p_2p_6$ ,  $p_2p_3p_4$  and  $p_4p_5p_6$ ) and then assemble them. For a detailed survey of decomposition methods, see [15].

Notice that, on the example of figure 1, if one removes one of the triangles, say  $p_2p_3p_4$ , and then tries to solve the remaining system, one needs to add information from the solved subsystem, otherwise the remaining system becomes articulated. This piece of information is called the border [23]. Although several methods exist to find the relevant information in specific resolution frameworks [28], no general algorithm yet exists to compute the border without adding too much information.

Indeed, it is important for resolution methods, especially for graph-based methods, that the system does not have too few or too many constraints. A system is said

- under-constrained if it has an infinite number of solutions because there are not enough solutions to pin down every geometric entity,
- over-constrained if it has no solution because of constraints redundancy,
- well-constrained if it has a finite positive number of solutions.

Invariance of rigid systems by displacements is generally taken into account by anchoring a point and a direction. The point and the direction are called a *reference* for the displacements. Other transformation groups may be considered [30].

A lot of work has been done about the detection of over-constrainedness [13, 27] or under-constrainedness [17, 18, 33, 37] and more generally about the characterization of rigidity [19, 20, 30, 35]. Yet, methods described in the literature are tricked by mathematical theorems when they are not explicitly taken into account in the construction of the resolution rules. Since a theorem list cannot be exhaustive, it is impossible to develop a rule-based or graph-based algorithm which detects geometric properties induced by mathematical theorems.

In this article, we extend the witness method [24] to address several problems cited above: how to determine the constrainedness level of a GCS without being tricked by mathematical theorems; how to efficiently detect all maximal well-constrained subsystems of a given GCS; how to decompose a well-constrained system into well-constrained subsystems.

This article is organized as follows: section 2 recalls the principles of the witness method and gives a way to generate a witness; section 3 demonstrates that an incremental version of the witness method has the same computational cost than the original version but allows to detect overconstrainedness in all cases; section 4 gives algorithms to efficiently identify the maximal rigid subsystems of an articulated system; section 5 deduces from these algorithms a method to further decompose a rigid system into rigid subsystems; finally, section 6 concludes and gives perspectives to this work.

## 2. THE WITNESS METHOD

### 2.1 Principle

The witness method comes from ideas of Structural Topology where the question of rigidity is studied through the notion of frameworks. A framework is a triple  $(V, E, p)$  where  $(V, E)$  is a graph and  $p : V \rightarrow \mathbb{R}^d$  a *realization of the graph*, which maps the vertices of  $V$  to points of dimension  $d$ . Thinking of graph edges as rigid bars and of vertices as articulation points, the main goal of combinatorial rigidity is to answer the question “Is  $(V, E, p)$  rigid?”.

*Infinitesimal flexion.* An *infinitesimal flexion* is a map  $q : V \rightarrow \mathbb{R}^d$  such that  $(p(i) - p(j)) \cdot (q(i) - q(j)) = 0$ , for each  $(i, j) \in E$ . A framework is called *infinitesimally rigid*, if the only flexions arise from the direct isometries of  $\mathbb{R}^d$ , *i.e.* the translations and rotations in 2D.

Under some conditions of genericity concerning incidence relationships, if one framework  $(V, E, p_0)$  is infinitesimally rigid then almost all frameworks  $(V, E, p)$  are infinitesimally rigid.

In other words, frameworks in rigidity theory correspond to the realization of a geometric constraint systems where all constraints are point-to-point distance constraints: such a system is generically well-constrained up to direct isometries if it is generically rigid. This was generalized by D. Michelucci et al.[26, 24, 25] to metric constraints over points, lines, etc.

*Witness.* Let  $F(X, A) = 0$  be a constraint system where  $X$  is the set of unknowns and  $A$  the set of parameters. We suppose that all constraints are of the form  $f(x, a) = 0$  and are differentiable. A *witness* is then a solution of  $F(X, A) = 0$  for some values of  $A$ .

Typically in CAD, when the designer draws a sketch, he/she yields a solution, say  $X_e$ , for system  $F(X, A_e) = 0$  where  $A_e$  are the values for  $A$  read on the sketch, since the goal is a solution for the system  $F(X, A_a) = 0$  where  $A_a$  are the values put on the dimensioning. Using a Taylor expansion for a small perturbation around a solution  $X_0$  for  $F(X, A_e) = 0$ , we have:

$$F(X_0 + \varepsilon v, A_e) = F(X_0, A_e) + \varepsilon F'(X_0, A_e) \cdot v + o(\varepsilon)$$

where  $v$  can also be seen as the instant velocity of each object involved in the system and  $\varepsilon$  is a small time step. Thus, if an infinitesimally small perturbation is another solution of  $F(X, A_e)$ , we must have

$$F'(X_0, A_e) \cdot v = 0$$

The space of the infinitesimal motions allowed by the constraints to the witness is then given by  $\ker(F'(X_0, A_e))$ . Note that

- the matrix  $F'(X_0, A_e)$  is known as the Jacobian of system  $F(X, A_e) = 0$  taken at point  $X_0$ ;
- when the constraints are all point-to-point distance constraints, this matrix is a minor of the rigidity matrix as defined in the combinatorial rigidity theory;
- for other constraints with parameter the genericity conditions are more complicated than in the combinatorial case: A parameter value  $A^*$  of a constraint  $f$  is called *generic*, if a solution  $X_{A^*}$ ,  $f(X_{A^*}, A^*) = 0$  with an open neighborhood  $\mathcal{S}(X_{A^*}, A^*)$  exists such that the

matrix

$$\begin{pmatrix} df(X, A)/dX & 0 \\ 0 & df(X, A)/dA \end{pmatrix}$$

has the same rank. It remains that the generic parameter values are dense in the set of parameter values corresponding to a realization. So a witness can be chosen by tacking coordinates at random, with probability 1 under the condition that the boolean constraints, typically incidence constraints, are satisfied.

We give some examples for the formulation of generic constraints. For point, line, plane incidences, we assume that the corresponding constraints are specified explicitly without parameters. This is to avoid expressing point-point incidences by a distance constraint  $(P_{1,x} - P_{2,x})^2 + (P_{1,y} - P_{2,y})^2 = d^2$  with distance parameter  $d = 0$ . For a distance constraint  $(P_{1,x} - P_{2,x})^2 + (P_{1,y} - P_{2,y})^2 = d^2$ , the parameter  $d = 0$  is not generic, as the constraint is singular in the solution point. For an angle constraint angle  $(P_1, P_2, P_3) = \theta$ , *i.e.*  $P_1 P_2 P_3 P_2 = l_{P_1 P_2} l_{P_3 P_2} \cos \theta$ , the parameter values  $\theta = \pm\pi$ ,  $\theta = \pm\pi/2$ , and  $\theta = 0$  are not generic. Similarly, point-line, line-line, line-plane and plane-plane incidence constraints are not expressed by angle constraints of non-generic angles.

Assuming that the constrainedness is generic for the constraint system  $S = F(X, A)$ , we can then study the degrees of freedom of  $S$  by studying the rank of the Jacobian  $F'(X_0, A_e)$  on a generic witness  $X_0$ , and in the case of under-constrainedness, the structure of the allowed infinitesimal motions can be deduced by the study of the kernel of  $F'(X_0, A_e)$ .

## 2.2 Generation of a witness

In principle, a witness solution can be determined by a solver for under-determined systems  $F(X, A) = 0$  like the subdivision solver presented in [7]. We replace the nonlinear monomials  $x_i^2$  and  $x_i x_j$  for  $i < j$  by additional variables  $x_{ii}$  and  $x_{ij}$ , which are enclosed in a polytope  $B_D(x_i, x_{ii}, x_{i,j,i < j}) \geq 0$  with halfspaces given by the non-negativity of relevant Bernstein polynomials (*Bernstein polytope*). The quadratic constraint system becomes a polyhedron  $S_D(x_i, x_{ii}, x_{i,j,i < j}) \geq 0$  after rewriting into the additional variables  $x_{ii}$  and  $x_{ij}$ . In this way, bounds for the solution domain of quadratic polynomials can be expressed as two linear programs

$$\begin{aligned} \min x_i \text{ and } \max x_i \\ S_D(x_i, x_{ii}, x_{i,j,i < j}) \geq 0 \\ B_D(x_i, x_{ii}, x_{i,j,i < j}) \geq 0 \end{aligned}$$

Domain bounds are computed by linear programming in order to reduce the current solution domain  $D$ . If the polytope is empty, which is detected by linear programming, then the current domain box contains no solution. Otherwise we can perform a sequence of reductions and bisections of domain boxes until the domain box  $D = [\underline{x}_1, \overline{x}_1] \times \dots \times [\underline{x}_n, \overline{x}_n]$  is  $\delta$ -small:  $(\overline{x}_i - \underline{x}_i) < \delta$  for all  $i$ . These  $\delta$ -small boxes cover the solution set piecewise.

The subdivision solver requires a domain box to start the search. The intervals for generic parameter values of constraints are easy to find: angle parameters  $\cos \theta$  ( $\cos \theta$  instead of  $\theta$  to avoid trigonometric functions in the solver) are in  $[-1 + \epsilon, -\epsilon]$  or  $[\epsilon, 1 - \epsilon]$  with a small, arbitrary  $\epsilon$ ; intervals for distance parameters  $d$  can be obtained from maximum bounds of the point coordinates. Finding a bound on the

magnitude of any root, is necessary to prove that the system has no solution. Such a root bound has been given in [36] and [1] for polynomial systems with a finite zero-set. In order to be in this case, it is necessary to divide by the common factors of the polynomials.

*Root bound [36].* Let  $f = (f_1, \dots, f_n)^t$  be a system of polynomials  $f_i \in \mathbb{R}[x_1, \dots, x_n]$  with total degree  $\text{tdeg}(f_i) = 2$  for  $i = 1, \dots, n$ . If the zero-set of  $f$  is finite, it holds for every root  $\xi = (\xi_1, \dots, \xi_n)^t \in \mathbb{C}^n$  that  $|\xi_i| < (2^{3/2} \alpha \beta)^\gamma 2^{(n+1)2^n}$ , where  $\alpha$ ,  $\beta$  and  $\gamma$  are given by

$$\begin{aligned} \alpha &= \max\{\sqrt{n+1}, \max_{1 \leq i \leq n} \|f_i\|_2\}, \\ \beta &= \binom{1+2n}{n}, \quad \gamma = \left(1 + \frac{n}{2}\right) 2^n. \end{aligned}$$

In order to enumerate all solutions of a system, we used mid-bisection of the largest interval in [7], which minimizes the height of the exploration tree while cycling through dimensions. For the case of determining a single solution as fast as possible, the choice of the smallest interval (greater or equal  $\delta$ ) is beneficial as setting variables to values allowing solutions improves the effectiveness of the domain reduction step.

In principle for a  $\delta$ -small box containing a solution, we need to check all subsets of three points  $P_1, P_2, P_3$  (in 2D) for degeneracy, *i.e.* for a zero determinant

$$\begin{vmatrix} P_1^t & 1 \\ P_2^t & 1 \\ P_3^t & 1 \end{vmatrix} = 0.$$

There are  $\binom{m}{3} \in \Theta(m^3)$  degenerate configurations for a system of  $m$  points but they are of zero measure inside the domain. In consequence for our bisection strategy, we start newly with a domain box containing a small neighborhood (a multiple of  $\delta$ ) of the solution found and change to the strategy, bisecting the largest interval. We compute  $n$  successive solutions and take the solution with largest rank of the Jacobian at the box center as a witness. This is similar to a perturbation of the solution in the space of infinitesimal motions to make it non-degenerate [24].

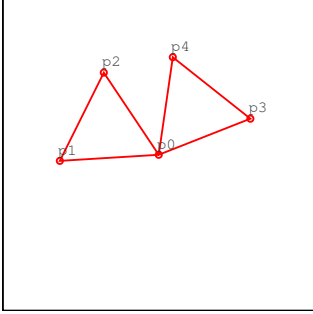
As examples, we show two systems of different difficulty. In Figure 2, two triangles with a common point  $p_0$  are specified by six side lengths. For the side lengths, the lower interval bound  $l = 0.01$  is found to admit a solution. In Figure 3, four points and five lines with 10 point-line incidences are specified by four angle parameters and a distance parameter. The left part shows a witness solution with symmetric and nice shaped triangles, obtained by additional minimum distance constraints between the triangle points. In the right part, a non-degenerate witness solution is shown, which was found without additional constraints automatically.

## 3. OVER-CONSTRAINEDNESS

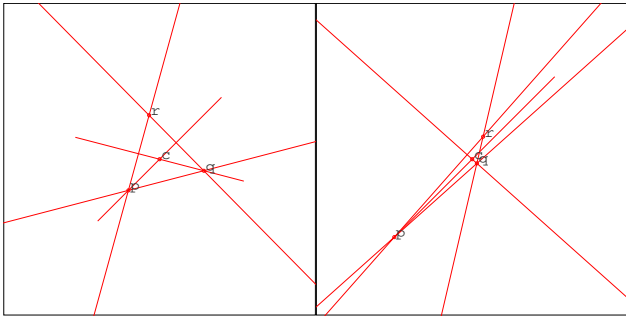
We already showed in section 1 that the detection of over-constrainedness is a complicated yet essential problem in the field of geometric constraints solving.

In this section, we show that the use of the witness method leads to an efficient and robust detection of redundancy in geometric constraints.

We also show the usefulness of the witness method to enhance robustness of decomposition methods by an accurate computation of the border.



**Figure 2: “The butterfly”:** 5 points with 6 distance parameter  $d(p_0, p_1)$ ,  $d(p_1, p_2)$ ,  $d(p_2, p_0)$ ,  $d(p_0, p_3)$ ,  $d(p_3, p_4)$ ,  $d(p_4, p_0)$ .



**Figure 3: System of 4 points and 5 lines with 10 point-line incidences, 4 angle parameter  $\text{angle}(qp, cp)$ ,  $\text{angle}(cp, rp)$ ,  $\text{angle}(rq, cq)$ ,  $\text{angle}(cq, pq)$  and 1 distance parameter  $d(r, c)$ . Symmetric witness solution (left) and random, non-degenerate witness solution (right).**

### 3.1 Incremental detection of over-constrainedness

We showed in [24] that it is possible to interrogate a witness in order to detect whether a set of constraints is dependent or not. Indeed, it is easy to compute the rank of the Jacobian matrix at the witness and to compare it with the number of constraints. However, finding a maximal independent subset of a dependent set is not a trivial problem. Working on the witness, the naive idea would be to try and remove constraints one by one and, at each step, compute the rank again to determine if the constraint is redundant with the remaining set. If the rank does not change, the constraint can be removed. Performed this way, the removal of redundant constraints is expensive. Yet, considering an incremental construction of the geometric constraint system allows to identify the set of redundant constraints with no additional costs in comparison to the basic detection of redundancy.

Indeed, consider a geometric constraint system  $\mathcal{S}$  with no redundancy between the constraints. Applying the Gauss-Jordan method on the Jacobian matrix at the witness leads to a matrix  $J' = IP$  with  $I$  a  $n \times n$  diagonal matrix and  $P$  a  $m \times n$  matrix,  $m$  being the number of actual degrees of freedom of the system. This method has a known complexity of  $\mathcal{O}(n^3)$ . Let us now consider a system  $\mathcal{S}'$  with  $\mathcal{S} \subset \mathcal{S}'$ . In order to know if  $\mathcal{S}'$  is over-constrained, one only needs to incrementally add the geometric entities and the constraints (bearing in mind that a constraint can be added only when the geometric entities it concerns are all in the system) of  $\mathcal{S}' - \mathcal{S}$  to  $\mathcal{S}$  and applying Gauss-Jordan again. Since the leftmost part of the matrix is the diagonal, the number of operations is at most  $2 \times n \times m$ : for each line of  $I$ , each non-zero element of  $P$  must be multiplied and added to the new line. The number of operation is in fact far smaller, since the number of zero elements in the new line of the matrix is high.

Proceeding incrementally does not raise the number of operations: it only changes the order of the operations. Indeed, the classical Gauss-Jordan method consists in column-by-column operations: for each column  $j$ , divide line  $j$  by  $J_{j,j}$ , then subtract  $J_{i,j}$  times this new line from line  $i$  for every  $i$ , so that column  $j$  is a null vector except for the  $j$ -th value. With the incremental calculus of the reduced row echelon form, one proceeds line by line: for each line  $i$ , subtract  $J_{j,i}$  times line  $j$  for each  $j < i$ , then divide line  $i$  by  $J_{i,i}$  so that the  $i - 1$  first elements of line  $i$  are zero and the  $i$ -th element is 1. Thus, the overall complexity of the incremental computation of the reduced row echelon form of  $J$  is also of  $\mathcal{O}(n^3)$ .

The incremental version of the Gauss-Jordan elimination has the same complexity as the global one, but has a major advantage in our case: at each step, when a constraint is added, one may compare the new rank with the previous one and thus detect a redundant constraint. With exactly the same number of operations as in the case of the classical Gauss-Jordan elimination, one obtains the reduced row echelon form of the Jacobian matrix together with the list of redundant constraints.

Let us consider the example of figure 4. The Jacobian matrix of this system is shown on table 1. Consider the following witness:  $p_1 = (2, 7)$ ,  $p_2 = (5, 6)$ ,  $p_3 = (1, 1)$  and  $p_4 = (6, 3)$ . The Jacobian at this witness is shown on table 2, with a partial Gauss-Jordan elimination, since the

Table 1: The Jacobian matrix for the system of figure 4.

	$x_1$	$y_1$	$x_2$	$y_2$	$x_3$	$y_3$	$x_4$	$y_4$
$r_1$ : dist( $p_1, p_2$ )	$x_1 - x_2$	$y_1 - y_2$	$x_2 - x_1$	$y_2 - y_1$	0	0	0	0
$r_2$ : dist( $p_1, p_3$ )	$x_1 - x_3$	$y_1 - y_3$	0	0	$x_3 - x_1$	$y_3 - y_1$	0	0
$r_3$ : dist( $p_2, p_4$ )	0	0	$x_2 - x_4$	$y_2 - y_4$	0	0	$x_4 - x_2$	$y_4 - y_2$
$r_4$ : dist( $p_3, p_4$ )	0	0	0	0	$x_3 - x_4$	$y_3 - y_4$	$x_4 - x_3$	$y_4 - y_3$
$r_5$ : dist( $p_2, p_3$ )	0	0	$x_2 - x_3$	$y_2 - y_3$	$x_3 - x_2$	$y_3 - y_2$	0	0
$r_6$ : dist( $p_1, p_4$ )	$x_1 - x_4$	$y_1 - y_4$	0	0	0	0	$x_4 - x_1$	$y_4 - y_1$

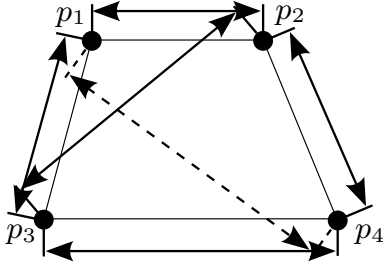


Figure 4: “The kite”: over-constrained 2D system with 4 points and 6 distances. Without the dotted constraint, the system is rigid.

Table 2: The Jacobian matrix of table 1 at a witness. The Gauss-Jordan elimination method was used on the first five rows. The sixth row is redundant ( $r_6 = r'_2 - r'_1$ )

	$x_1$	$y_1$	$x_2$	$y_2$	$x_3$	$y_3$	$x_4$	$y_4$
$r'_1$	1	0	0	0	0	$-\frac{1}{\ x_3 - x_1\ }$	-1	$-\frac{y_3 - y_1}{\ x_3 - x_1\ }$
$r'_2$	0	1	0	0	0	$-\frac{y_3 - y_1}{\ x_3 - x_1\ }$	0	$-\frac{1}{\ x_3 - x_1\ }$
$r'_3$	0	0	1	0	0	$-\frac{1}{\ x_2 - x_4\ }$	-1	$-\frac{y_2 - y_4}{\ x_2 - x_4\ }$
$r'_4$	0	0	0	1	0	$-\frac{1}{\ x_2 - x_4\ }$	0	$-\frac{y_2 - y_4}{\ x_2 - x_4\ }$
$r'_5$	0	0	0	0	1	$\frac{1}{\ x_3 - x_2\ }$	-1	$-\frac{y_3 - y_2}{\ x_3 - x_2\ }$
$r'_6$	-1	1	0	0	0	0	1	-1

sixth line has not been modified. That is, table 2 shows the matrix obtained by performing the incremental version of the Gauss-Jordan elimination, after adding the sixth constraint but before performing the elimination on it. It is easy to see that the sixth row is redundant, since it can be obtained by subtracting the first row from the second one. Thus, we detected the over-constrainedness.

For a more complex and famous example, consider the double-banana (see figure 5): adding the last constraint of the double-banana leads to a zero-filled line in the Jacobian matrix at the witness. If one considers an example with higher connectivity [22], our method still succeeds to efficiently detect over-constrainedness.

Moreover, the witness method manages to detect cases of under-constrainedness for which graph-based methods are helpless because they do not consider geometric theorems. For instance, consider the example in figure 6. It is unlikely that a graph-based method can ever detect the fact that point  $y$  is fixed, no matter what coordinates are given to point  $p$  and line  $l$ . Hence, a graph-based method would see this system as a system with 8 remaining degrees of freedom (5 for the three aligned points  $a, b$  and  $x$ , 1 for line  $l$  traversing  $x$  and 2 for point  $p$ ) and would consider that adding a constraint distance between points  $a$  and  $y$

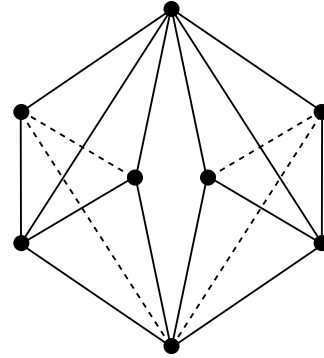


Figure 5: “The double-banana”: famous counterexample to the extension of Laman’s characterization of rigidity in 3D. Each segment represents a distance constraint.

removes a degree of freedom. The witness method, however, detects that this new distance constraint is redundant.

### 3.2 Accurate computation of border systems

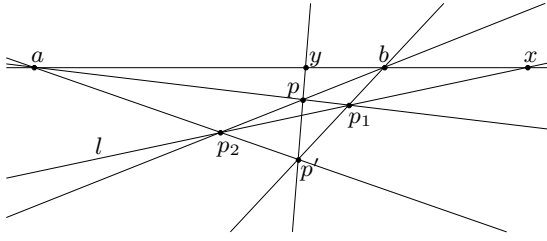
This easy and efficient way to compute a maximal independent subset is also useful in decomposition to make sure that the border of a subsystem is not over-constrained.

Recall that the border of a system  $S'$  according to a system  $S$  is the set of all information computable in  $S'$  about geometric entities which are both in  $S$  and  $S'$ . For instance, if  $S'$  is a rigid system which shares three points with system  $S$ , then the border of  $S'$  contains the following displacement-invariant constraints:

- the three point-point distances,
- the three angles between the sides of the triangle.

It is easy to see that if the border of a subsystem is not added after removal of the subsystem from a rigid GCS, then the remaining GCS becomes under-constrained because information is lost. For instance, consider the GCS of figure 4 without the constraint shown with dotted lines. The triangle  $p_1p_2p_3$  is rigid and trivially solved. If it is removed from the system, the remaining GCS is a 2-bars system containing two distance constraints:  $p_3 - p_4$  and  $p_2 - p_4$ . This remaining system has solutions which are not subfigures of the global GCS, since the angle between both bars may vary.

To get rid of this problem, one may add the border of the solved subsystem to the remaining system [23]. In the example above, the border of triangle  $p_1p_2p_3$  consists in the distance between points  $p_2$  and  $p_3$ . With a bigger border, a new problem arises. Consider, for instance, a rigid subsystem which shares three points with the remaining system. One can compute the values of the three point-point



**Figure 6: Given three aligned points  $a, b$  and  $x$  and for any point  $p$  and line  $l$  traversing  $x, y$  is unchanged:  $p_1 = (ap) \cap l, p_2 = (bp) \cap l, p' = (ap_2) \cap (bp_1), y = (ab) \cap (pp')$ .**

distances, but also the values of the three angles. Thus, the border is an over-constrained GCS with three points and six constraints. Although, formally, the system is not over-constrained since the metrics are consistent, it is structurally over-constrained, which means that any combinatorial method will fail to continue the solving process.

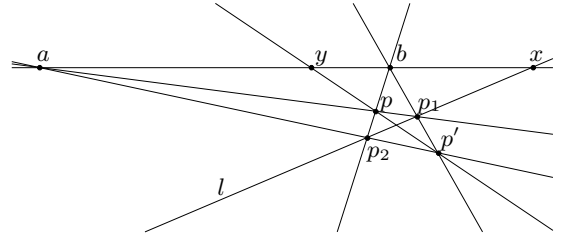
Using our incremental Gauss-Jordan elimination method, one can compute a well-constrained subset of the border system which contains all the information to generate the rest of the border system. One adds all the constraints of the border one by one to an empty system. If the last added constraint is redundant with the previous ones, one removes it.

#### 4. DETECTION OF MAXIMAL RIGID SUBSYSTEMS IN ARTICULATED SYSTEMS

In this section, we show how the witness method can be used to efficiently detect all maximal rigid subsystems (MRS) of a geometric constraint system, even with systems for which graph-based methods would fail to detect rigidity. We give a basic algorithm based on a series of Gauss-Jordan eliminations then show two ways to enhance computation speed.

The basic idea of our MRS detection algorithm is to study which geometric entities are fixed when one anchors a reference for the displacements (see [30] or [23] for a formal definition of references). In the witness framework, anchoring a reference for the displacements consists in switching columns in the Jacobian matrix so as to put the three columns of the reference in the right-most positions. Indeed, performing a Gauss-Jordan elimination diagonalizes the matrix from the left and thus consists in expressing the different coordinates as functions of the right-most columns (the ones that do not belong to the identity part of the matrix). For instance, table 2 shows the reduced row echelon form of the Jacobian matrix at the witness for the GCS of figure 4. Since this GCS is rigid (once the redundant constraint removed), three columns do not belong to the identity part of the matrix: they correspond to coordinates  $x_4, y_4$  and  $y_3$ , which form a reference for the system. All other coordinates can be expressed in function of these three coordinates. For instance, the first line of the matrix must be interpreted as  $x_1 - \frac{4}{5} \times y_3 - x_4 + \frac{4}{5} \times y_4 = 0$ , *i.e.*  $x_1 = \frac{4}{5} \times y_3 + x_4 - \frac{4}{5} \times y_4$ .

When the GCS is not rigid, three parameters are not enough to anchor all entities. There are then more than three columns at the right of the identity. Table 3 shows the reduced row echelon form of the Jacobian matrix at a witness for the GCS of figure 7. Notice that columns  $y_2$  and  $y_4$  were moved to the right, since it would have been impos-



**Figure 7: Articulated chain made of three rigid triangles. Distance constraints are implicitly represented by the segments.**

sible to find a pivot and finish the Gauss-Jordan elimination otherwise. All coordinates can be expressed as functions of  $y_2, y_4, y_6, x_7$  and  $y_7$ . Indeed, a reference for this GCS can consist in point  $p_7$ , direction  $p_7-p_6$ , direction  $p_5-p_4$  and direction  $p_3-p_2$ .

An important result to identify MRSs comes from the zeros in columns  $y_2$  and  $y_4$ . Rows 7, 8 and 9 of table 3 can be interpreted as the fact that the values of  $x_5, y_5$  and  $x_6$  depend only on those of  $y_6, x_7$  and  $y_7$ . Said otherwise, if one anchors a reference for the displacements by pinning down  $p_7$  and direction  $p_7-p_6$ , then points  $p_6$  and  $p_5$  are fixed, *i.e.*  $p_5p_6p_7$  is a rigid subsystem.

A naïve algorithm immediately arises, based on anchoring a reference for the displacements, *i.e.* switching columns to have the corresponding columns on the right of the Jacobian matrix and identifying the parts of the GCS which are fixed. The pseudo-code is shown at algorithm 1. In this algorithm, anchoring a reference for the displacements means switching columns so as to have the columns corresponding to the reference at the right of the Jacobian matrix. In order not to identify the same MRS twice, we anchor references only on untagged parts of the GCS, that is to say that at least one of the columns cannot be tagged.

The cost of this algorithm depends on the number  $m$  of MRSs: for each of them, one performs once and only once a Gauss-Jordan elimination, that is to say that the total cost is  $\mathcal{O}(m \times n^3)$ .

This cost can be reduced by not starting the Gauss-Jordan elimination from scratch for each MRS. At the end of line 6 in the algorithm, the Jacobian matrix at the witness is under reduced row echelon form. By switching the columns

**Table 3: Reduced row echelon form of the Jacobian matrix at a witness for the GCS of figure 7**

	$x_1$	$y_1$	$x_2$	$x_3$	$y_3$	$x_4$	$x_5$	$y_5$	$x_6$	$y_2$	$y_4$	$y_6$	$x_7$	$y_7$
$r'_1$	1	0	0	0	0	0	0	0	0	$\frac{4}{3}$	$\frac{101}{18}$	$-\frac{181}{108}$	-1	$-\frac{473}{108}$
$r'_2$	0	1	0	0	0	0	0	0	0	$-\frac{7}{3}$	$-\frac{40}{9}$	$\frac{28}{27}$	0	$\frac{140}{27}$
$r'_3$	0	0	1	0	0	0	0	0	0	4	$\frac{29}{2}$	$-\frac{15}{4}$	-1	$-\frac{59}{4}$
$r'_4$	0	0	0	1	0	0	0	0	0	0	$\frac{17}{3}$	$-\frac{17}{12}$	-1	$-\frac{37}{12}$
$r'_5$	0	0	0	0	1	0	0	0	0	0	$\frac{5}{3}$	$-\frac{7}{12}$	0	$-\frac{35}{12}$
$r'_6$	0	0	0	0	0	1	0	0	0	0	3	$-\frac{7}{12}$	-1	$-\frac{11}{6}$
$r'_7$	0	0	0	0	0	0	1	0	0	0	0	$-\frac{5}{6}$	-1	$-\frac{5}{6}$
$r'_8$	0	0	0	0	0	0	0	1	0	0	0	$-\frac{5}{6}$	0	$-\frac{5}{6}$
$r'_9$	0	0	0	0	0	0	0	0	1	0	0	$-\frac{5}{6}$	-1	$-\frac{5}{6}$

---

**Algorithm 1** Naïve MRS identification algorithm

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- 1:  $i \leftarrow 0$
  - 2: **repeat**
  - 3: anchor a reference for the displacements on an untagged part of the GCS
  - 4: perform a Gauss-Jordan elimination
  - 5: tag with label  $i$  the columns of the GCS which correspond to coordinates depending only on the reference
  - 6:  $i \leftarrow i + 1$
  - 7: **until** all the columns are tagged
- 

in an appropriate way, one needs only perform the Gauss-Jordan pivot operation on two to three columns. Indeed, by looking at the constraint graph, it is possible to select a new reference for the GCS (*i.e.* a set of  $n$  columns,  $n$  being the number of degrees of displacement of the GCS) which satisfies the following conditions:

- it includes a reference for the displacements which is not totally tagged,
- each identified MRS is fixed, *i.e.*
  - the reference includes three coordinates in the MRS,
  - the MRS shares a point with a fixed MRS and the reference includes a coordinate in the MRS.

To select this reference, one only needs to consider a point which is in an already identified MRS and which is linked by a constraint to an untagged entity. More cases occur with systems for which the constraint graph has several connected components or with systems with implicit points (*e.g.* similarity-invariant systems with only lines and angles), but the principle remains. Thus, in most cases, one only needs to switch two columns, so as to change the point in the reference. Three switches happen with disconnected graphs. Algorithm 2 shows how to perform MRS identification. For the sake of simplicity, the algorithm works only on articulated GCS made of several MRSs connected by points.

In the case of open chains, *i.e.* GCS where all cycles in the constraint graph are included in rigid subsystems, an even less costly algorithm exists, by using both the constraint graph and the Jacobian matrix. After performing the Gauss-Jordan elimination, a first MRS is identified by considering all the coordinates which depend only on the reference. From there, one can consider all the coordinates which depend on the reference and on one additional parameter. In the matrix of table 3, with the additional parameter

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**Algorithm 2** MRS identification algorithm for an articulated system

---

- 1: anchor a reference for the displacements and identify a first MRS
  - 2: **repeat**
  - 3: select a tagged point linked by a constraint to an untagged element
  - 4: switch the columns of this point with the columns of the point in the last reference
  - 5: perform Gauss-Jordan elimination on the two latter
  - 6: **until** all the columns are tagged
- 

$y_4$ ,  $x_3$ ,  $y_3$  and  $x_4$  are fixed. Taking a look at the constraint graph, we notice that the previously identified MRS ( $p_5p_6p_7$ ) shares only one point with the rest of the system and thus cannot “transfer” more than two degrees of displacement.

This enables us to remove the MRS and exchange the three parameters  $y_6$ ,  $x_7$  and  $y_7$  with parameters  $x_5$  and  $y_5$  in the Jacobian matrix. The numerical values are not important in this process: we consider that all the values of both columns are non-zero. With this new matrix, one notices that parameters  $x_5$ ,  $y_5$  and  $y_4$  form a reference for the displacements and that by anchoring this reference,  $x_3$ ,  $y_3$  and  $x_4$  are fixed, *i.e.*  $p_3p_4p_5$  is a rigid system. We continue this algorithm by noticing that this system shares only one point with the rest of the system, removing it and replacing it with non-zero-filled columns  $x_3$  and  $y_3$  and thus identifying the last MRS  $p_1p_2p_3$ .

When the last identified MRS shares more than one point with the rest of the system, two cases occur: either the removal of the MRS leads to two disconnected graphs (*i.e.* the MRS is in the middle of the articulated system) and one thus continues the algorithm separately on each part of the graph; or the MRS belongs to a non-rigid closed chain.

When one uses this algorithm on a GCS containing non-rigid closed chains, it leads to cases where one cannot detect the MRSs of the closed chains, because of the interdependence of the rigid subsystems of the chain: after identifying the first MRS of the closed chain, the algorithm is stuck because it is not possible to identify another system which depends only on three parameters. In this case, we get back to algorithm 2 to identify the different MRSs of the closed chain.

Notice that this section is about identification of maximal rigid subsystems but that since it is based on the anchoring of references, one may adapt the algorithms to identify maximal subsystems well-constrained *modulo* other transformation groups than the displacements.

## 5. W-DECOMPOSITION OF A RIGID GCS

In the last section, we gave algorithms to identify all MRSs of a GCS. Having such an algorithm leads to a natural method to decompose a rigid geometric constraint system. We call this method W-decomposition and a system which can be decomposed by this method is said W-decomposable. In this section, we explain the principles of W-decomposition and give examples.

Algorithm 2 identifies maximal rigid subsystems, *i.e.* if a MRS can be decomposed in several rigid subsystems, this will not be detected. The basic idea of W-decomposition is to remove edges from the constraint graph and see if it breaks the MRS in non-trivial MRSs, *i.e.* MRSs which are not limited to their border. If it does, then we use W-decomposition on each non-trivial MRS. Algorithm 3 gives the pseudo-code of the algorithm.

---

### Algorithm 3 W-decomposition

---

**Input:** a rigid GCS  $\mathcal{S}$  with  
its constraint graph  $G = (V, E)$  and  
a witness  $W$  of  $\mathcal{S}$

**Output:** a list of rigid subsystems

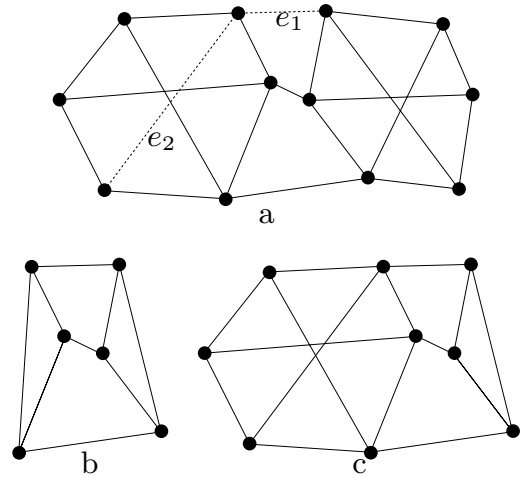
- 1: **repeat**
- 2:   Delete an edge  $e$
- 3:   Identify MRSs of  $(V, E/\{e\})$  with alg. 2
- 4:   **while** each MRS is equivalent to its border **do**
- 5:     Choose another edge  $e$  and identify MRSs of  $(V, E/\{e\})$
- 6: **until** all edges were tested or there is a MRS which is not equivalent to its border
- 7: **if** no MRS bigger than its border was found **then**
- 8:   return list  $[G]$  //  $G$  is  $W$ -indecomposable
- 9: **else**
- 10:   remove all the constraints included in non-trivial MRSs
- 11:   add the border of all non-trivial MRSs //cf. *section 3.2*
- 12:   reintroduce edge  $e$  // *this gives a rigid constraint system*
- 13:   recursively W-decompose the resulting system
- 14:   recursively W-decompose all previously identified MRSs
- 15: **return** the concatenation of the lists obtained in the last two lines

---

Let us illustrate this algorithm on the example of figure 8a, which represents the constraint graph of a rigid GCS. The graph is 3-connected and has two  $K_{3,3}$  subgraphs, connected by three “middle” edges. Algorithm 2 detects the rigidity of the whole system. Let us consider the removal of two edges at line 2 of algorithm 3: dotted edges  $e_1$  and  $e_2$ .

If we remove edge  $e_1$ , the use of algorithm 2 at line 3 identifies four MRSs: the rigid  $K_{3,3}$  subsystems, and each edge between them. The latter are equivalent to their border. Replacing the rigid hexagons by their borders and reintroducing edge  $e_1$  leads to the graph of figure 8b (note that edge  $e_1$  must be taken into account for the computation of the borders). The recursive use of W-decomposition (line 14) on each non-trivial MRS leads to the knowledge that they are not W-decomposable, as does the recursive use on the system of figure 8b (line 13).

If we do not remove edge  $e_1$  but  $e_2$  instead, the left  $K_{3,3}$  subsystem is no longer rigid. The identification of non-trivial MRS thus only identifies the right hexagon. Once



**Figure 8:** a: 3-connected constraint graph made of two  $K_{3,3}$  graphs connected with 3 constraints; b and c: graphs obtained by replacing MRSs identified by algorithm 3 by their border with respectively edges  $e_1$  and  $e_2$  removed.

it is replaced by its border, we obtain the system shown on figure 8c. The recursive use of W-decomposition will then lead, after removal of one of the three “middle” edges, to the identification of the second rigid hexagon and thus to the system shown on figure 8b.

Efficiency of the execution depends on the choice of the edge to remove. In the worst case, all edges are tested:  $2 \times n - 3$  uses of algorithm 2 are made, this the complexity is  $\mathcal{O}(n^4)$ .

Our algorithm is more powerful than algorithms found in the literature, for several reasons:

- first of all, it is independent of the connectivity of the constraint graph. For instance, figure 9a gives an example of a 4-connected constraint graph which is W-decomposable, no matter what is inside the inner blue part as long as it is rigid,
- second, it is also not based on a cluster formation. Since the graph of figure 9b is not decomposable by current graph decomposition methods, the system of figure 9a, with the inner part replaced by figure 9b, will also lead to a decomposition failure for these methods, whereas it is W-decomposable.

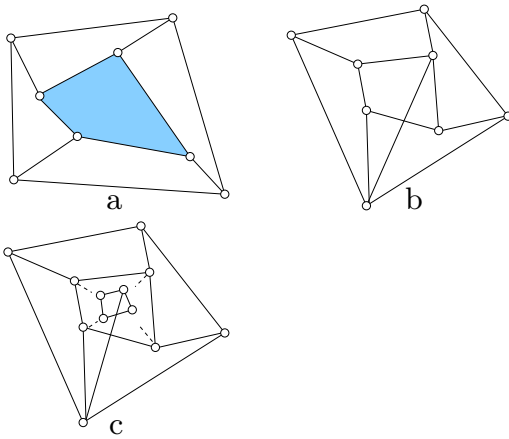
Unfortunately, it is easy to construct an infinite family of W-indecomposable constraint systems like the one depicted on figure 9c.

## 6. CONCLUSION

After proposing a way to generate a witness, we showed in this paper how the witness method could be used to detect over-constrained systems without any additional computational cost, through an incremental Gauss-Jordan elimination in the Jacobian matrix at the witness. This allows us to ensure the robustness of decomposition methods by a computation of a well-constrained border.

We gave algorithms to identify all maximal well-constrained subsystems of a GCS, *i.e.* the system itself if it is well-constrained, or its rigid parts if it is articulated. From this





**Figure 9: Examples for the W-decomposition: each vertex is a point and each edge represents a distance constraint. a: W-decomposable 4-connected GCS (the blue subsystem is rigid); b: W-indecomposable system; c: there are W-indecomposable systems with an arbitrary number of points.**

algorithm, we deduced a method, called W-decomposition, to decompose a rigid GCS into the set of all its non-trivial rigid subsystems, based on the removal of a constraint and the computation of the new maximal rigid subsystems.

The method to detect over-constrainedness is efficient (the computation of the reduced row echelon form of the Jacobian matrix is performed in  $\mathcal{O}(n^3)$ ) and is not tricked by mathematical theorems, even when these theorems are unknown to the developer. The MRS identification is also efficient ( $\mathcal{O}(n^3)$  with algorithm 2) and works as well with other transformation groups than the displacements. W-decomposition is performed in  $\mathcal{O}(n^4)$  in the worst case.

Further research needs to be done in order to find heuristics for the optimization of W-decomposition. The example of figure 8 shows that some edges are better than others for the removal (line 2 of algorithm 3). We believe that a promising track is that of the computation of a minimum chain covering and the research of edges which appear in few chains.

We also intend to further investigate the overconstrainedness detection method. Indeed, when a constraint is identified as redundant, the user may want to know why it is redundant, that is to say what are the minimal sets of vectors needed to generate the redundant one.

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